



Inelastic Behavior of Materials

prepare by:

Saman Mustafa Kamal Mawlana

B.Sc. Civil Engineering (۲۰۰۳)

MBA (۲۰۱۴)

M.sc. Student Structural Engineering

ID No. ۶۵۷۸

Saman_ceng@yahoo.com

+۹۶۴ (۰) ۷۷۰ ۱۵۷۳۷۱۶

+۹۶۴ (۰) ۷۵۰ ۱۵۷۳۷۱۶

۲۰۱۷

Contents

1. Introduction	3
1.1. Objective	4
2. Difference between Plastic and Elastic	4
2.1 Comparison between Plastic and Elastic:	6
3. MALLEABILITY AND DUCTILITY	7
3.1 Non-Adaptive Displacement-Based Pushover:	13
3.2 The Displacement-Based Adaptive Pushover Algorithm (DAP)	14
3.3 Capacity curves:	14
3.4 CREEP FAILURE	14
4. Conclusions:	15
5. References:	16

1. Introduction

Materials are the driving force behind the technological revolutions and are the key ingredients for manufacturing. Materials are everywhere around us, and we use them in one way or the other. The materials and the manufacturing process employed, could be better appreciated if one understands various types of materials and its properties [1].

define the inelastic behavior is Deformation of a cloth that continues to be even once the force that caused it's been mitigated or removed. several structural failures of ferroconcrete structures throughout earthquakes square measure because of the poor behavior of the structures within the inelastic vary [2].

The effects of inelastic behavior were 1st explored in metal structures and later utilized in their analysis and style. the character of inelastic deformations of ductile metals, the flow and dislocation processes concerned in it, square measure by currently moderately well understood. it's additionally established that restricted amounts of such inelastic deformations do no injury to strength and structure of ductile metals, a minimum of in their resistance to considerably static masses [3].

In ferroconcrete structures, once spring less flexural behavior of the members is caused primarily by yielding of the reinforcement, the information and assurance simply mentioned in relation to metal structures applies here still. this case, wherever spring less deformations square measure caused primarily by plastic flow within the reinforcement, obtains in members with steel ratios that are little as compared to the balanced ratios. However, the arrival of upper strength reinforcements and therefore the tendency to lighter and additional slender members create higher steel ratios, not abundant below the balanced values, economically more and more engaging. For such ratios, considerably spring less behavior. of continuous structures involves giant concrete strains. That is, below such conditions spring less behavior and moment distribution need the concrete to operate in this vary of strains wherever its response as a fabric is essentially spring less [4].

This poses the question of the character of dead deformations in concrete, of attainable changes in internal structure caused by such deformations, of effects of such changes on the integrity of concrete therefore strained, and of the fracture mechanism of concrete. it's believed that an accountable development of dead ways of style and analysis, significantly once applied to high-strength steels and concretes, cannot proceed while not such background data on the character of dead behavior and fracture of concrete [5].

The presence of microscopic cracks and therefore the progression of internal rending in concrete specimens in compression was initial suspected by Brandtzaeg in 1929 He ascertained the volumetrically changes of plain concrete cylinders in concentrically compression and located that at "critical load," (77- 90) % of the most load, the degree

started increasing instead of to continue decreasing. His conclusion was that failure progressed by internal rending in microscopic regions distributed throughout the fabric. within the same work it had been surmised that the form of the stress-strain curve was concerning this internal rending, which the curvature was thanks to the fast growth of the fabric [٦].

This study introduces the concepts of inelastic behavior, explains why the behavior is expected in seismic response.

١.١. Objective

These are the main objectives of the topic.

- Illustrates inelastic behavior of materials and structures
- Explains why inelastic response may be necessary

In the first part of this study, we work through a “hierarchy” of behavior from material, to cross-section to critical region and finally critical region, In earthquake engineering, inelastic response is expected, and survivability of structures depends on the ability of the structure to sustain several cycles of fully reversed inelastic deformation without excessive loss of stiffness or strength.

٢. Difference between Plastic and Elastic

The main difference between a plastic body and an elastic body is based on individual their ability to regain their shape and size after an external force is applied to the bodies [٧].

Both, elastic and plastic materials are widely applicable and used in the field of science and technology. Thus, it is easier to understand these properties in terms of physics.

Generally, the terms ‘plastic’ and ‘elastic’ are, physical properties, used to describe an object. They describe the attributes of materials such as rubber, plastic, metal, etc. In physics, when an external force is applied to the surface of any material or a body, the material undergoes a physical change or deformation. Now, when the force is removed, the material depending on its properties may or may not return to its original shape.

Now, if the body returns to its original shape, the body is said to be elastic in nature, and this property is called as ‘elasticity’. On the other hand, if the body does to regain its original shape, the body displays plastic nature, and this property is termed as

'plasticity'. Based on the above explanation, it becomes easier to define the two properties, and state the difference between them.

Elasticity is a property of a material to be flexible or buoyant in nature. When an external force is applied to a body, the body falls apart. This happens because the distance between the lattice atoms increases and each atom tries to pull its neighbor closer to itself. The pull creates a force in the material which tries to resist the deformation. This force is termed as strain, and the deforming force is termed as stress. Although, it is a reversible property, there is a limit to the magnitude of the force which is applied to the body. This limit is called the elastic limit of a body.

The 'elastic limit' of a body is defined as the maximum extent to which a solid may be stretched without permanent deformation. This property can be easily explained on the basis of Hooke's law. The law states that, the elasticity of that material depends on the ratio of the stress and strain acting on the body.

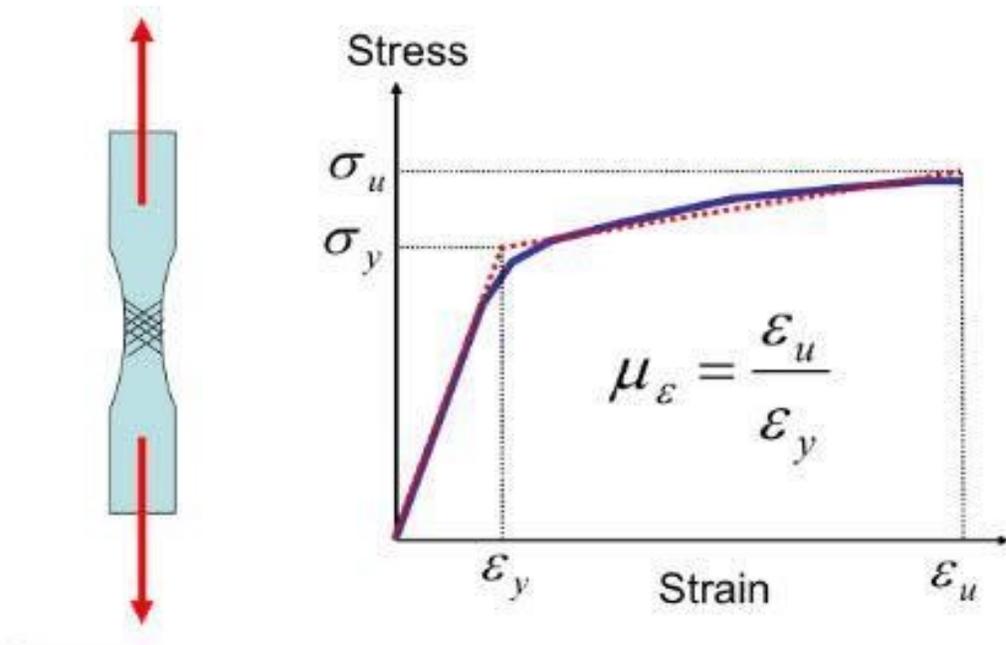
Which means, if the applied stress is linear or equal to the strain on the body, then body is under elastic limit, and is elastic in nature. But, when the force or stress on the body increases and the elastic limit is broken, the body becomes deformed and turns plastic in nature. This limit is known as the yield strength of the material, wherein an elastic body turns plastic in nature.

Plasticity is defined as the ability of a body to change its shape and size permanently, when an external force is applied. In a plastic body, when a force is applied, from the many layers of atoms, two of these layers' slide from their crystal planes, and lose their elastic limit, which causes the deformation in the body.

Based on the above explanation, one can say that a change in these properties only happen, when a body undergoes elastic deformation to enter plastic deformation. Thus, it can be said that both these properties are inter-related. Further differences between the two can be read in the table below.

2.1 Comparison between Plastic and Elastic:

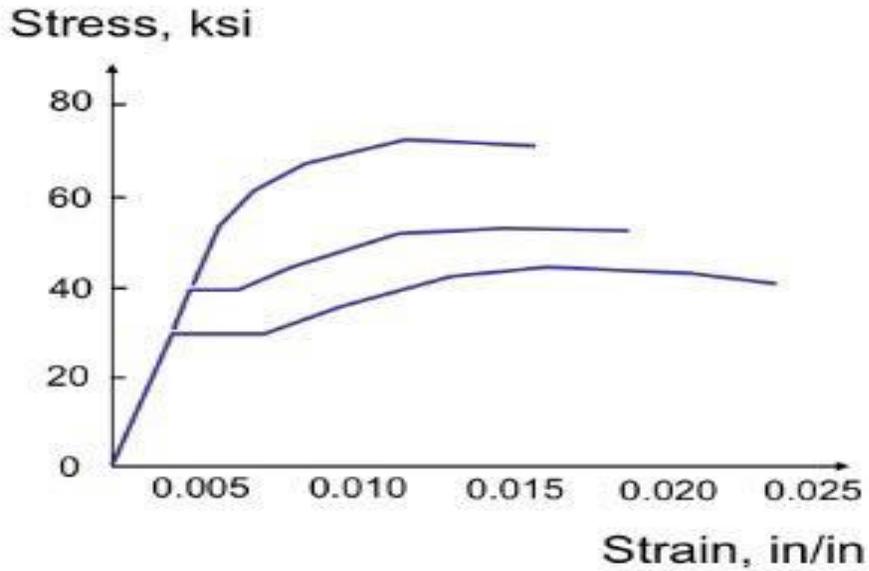
	Plastic	Elastic
Definition	The property on account of which a body does not regain its original size and shape on removal of applied force is called as plastic body.	The property on account of which a body regains its original size and shape on removal of external deforming force is called as elastic body.
Process	It is irreversible.	It is reversible.
Ductility	They are highly ductile in nature.	It is less ductile in nature.
Resilience	They have low yield strength.	They have high yield strength.
Modulus of elasticity (ratio)	The ratio of stress to strain is high.	The ratio of stress to strain is low or equal.
Toughness	They do not have the ability to absorb energy up to a fracture.	They have the ability to absorb energy up to a fracture.
Bonds	The molecular bonds are fractured.	The molecular bonds do not get fractured.
Shape and size	The shape and size changes permanently.	The shape and size does change permanently,



Idealized Inelastic Behavior from Material

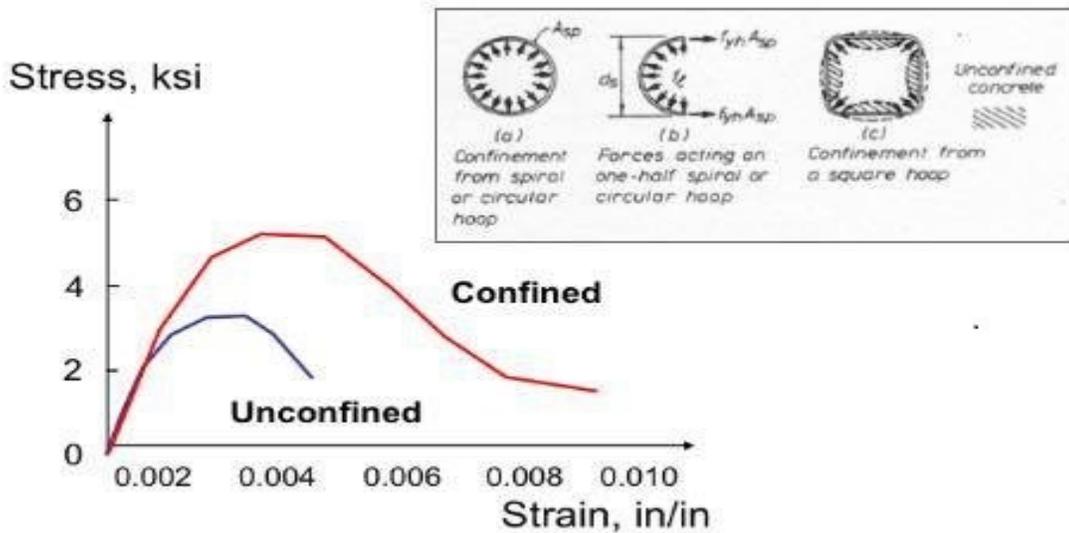
2. MALLEABILITY AND DUCTILITY

Both these properties relate to the malleability of the fabric. physical property refers to the power of plastic deformation below compressive masses, whereas plasticity refers to plastic deformation below tensile masses. A malleable material will be crushed into skinny sheets and even agent foils. A ductile material will be drawn into wires. A steel coupon is being tested, and therefore the stress-strain curve is planned. The stress and strain at yield is straightforward to spot for low strength steel, but may be harder to spot for higher strength steel. The ultimate stress is often taken because the most come-at-able stress, and the corresponding most strain is recorded. The malleability offer, in terms of strain, is adequate the most come-at-able strain divided by the yield strain. This malleability offer should be larger than that demanded by the earthquake [^].



Stress-Strain curve for Steel

A series of stress-strain curves square measure shown for steel. As stated previously, the yield stress is far easier to spot for the lower strength steels [9].



Stress-Strain curve for Concrete (Unconfined and Confined)

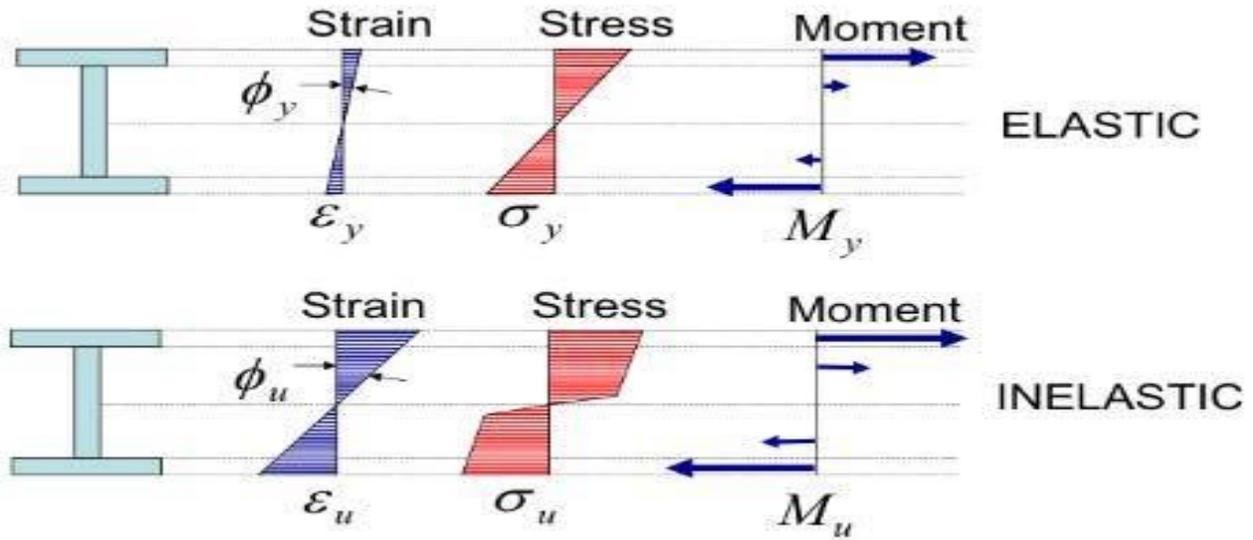
An example of a brittle material with totally different properties in tension and compression is provided by concrete, whose stress-strain diagram is shown. On the strain aspect of the diagram could be a linear elastic place that the strain is proportional to the strain. once the yield purpose has been reached, the strain will increase quicker than the strain till rupture happens. The behavior of the fabric in compression is totally different. First, the linear elastic vary is considerably larger. Second, rupture doesn't occur because the stress reaches its most price. Instead, the strain decreases in magnitude whereas the strain keeps increasing till rupture happens. Note that the modulus of physical property, that is portrayed by the slope of the stress-strain curve in its linear portion, is that the same in tension and compression. this is often true of most brittle materials [10].

The stress-strain curve for concrete is very addicted to the confinement of the concrete. below high confinement (as applied by fluid mechanics pressure, for example), there's Associate in Nursing considerable increase in strength and deformation capability. In earthquake engineering, the big increase in deformation capability is very necessary. If concrete strains were restricted to zero.003 or 0.004, concrete couldn't be employed in seismic areas. In ferroconcrete structures, confinement is provided passively by closely spaced reinforcement, sometimes provided within the style of hoops. once the section is below compression, Poisson's impact is to supply lateral growth. The stiffer confining reinforcement restrains this growth, thereby applying confining pressure [11].

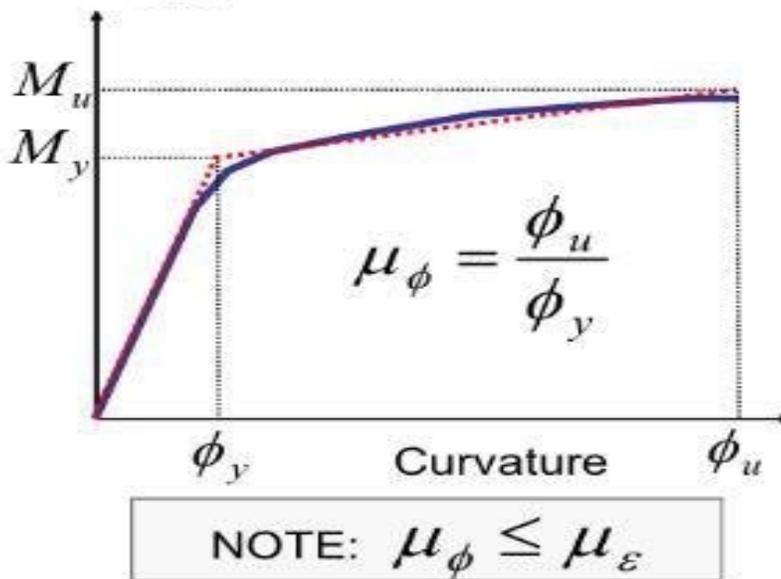


Circular spirals confine concrete far more effectively than one-dimensional ties. The helpful effects of circular spiral steel reinforcement embrace strength sweetening, a rise in strain admire most strength, and a greatly exaggerated ability of the concrete to sustain giant deformations while not vital strength loss. once concrete sections square

measure subjected to giant deformations, as an example underneath earthquake conditions, their ability to hold masses depends totally on the strength and deformation characteristics of the confined concrete. many influencing variables are thought of, as well as the diameter, spacing, and yield strength of the spiral reinforcement. The spacing of the spiral reinforcement has been known joined of the prime variables. thought has conjointly been given to the quantitative relation of the spacing of the spirals to the diameter of the confined core [12].

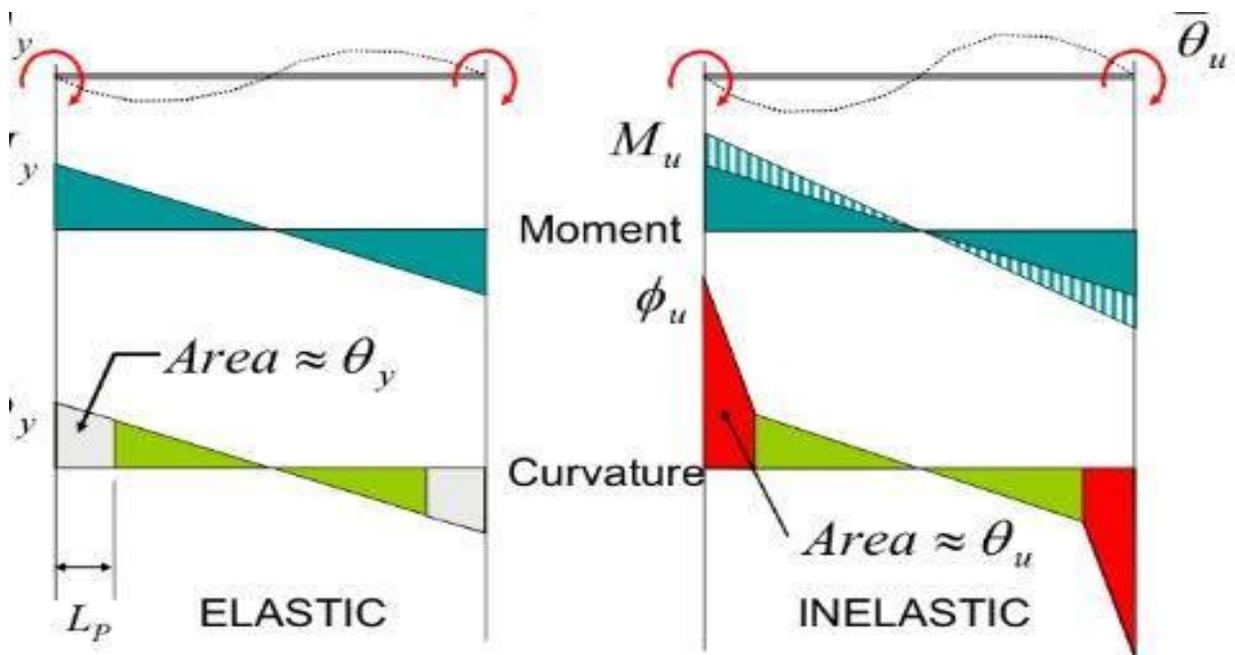


Elastic and Inelastic Behavior in Section



Moment curvature in Inelastic Behavior to Section

The moment-curvature relation for the section is shown. Again, it is important to note that the ductility indicated is the ductility SUPPLIED by the cross section. Use of confining steel in the critical regions of columns designed for earthquake resistance is a common way of achieving ductile structural behavior. The lateral steel, in conjunction with the longitudinal steel, affects the concrete properties significantly depending on several factors, which include distribution of steel including spacing of longitudinal and lateral steel, amount of lateral steel, and the type of anchorage of lateral steel. In addition, the mobilization of concrete confinement is affected by the strain gradient caused by flexure. In general, a conservative evaluation of the capacity is considered safe. However, in the capacity design approach [1], for seismic considerations, an underestimation of flexural capacity may result in a brittle shear fracture even when the members are well detailed for ductile flexural behavior[13].

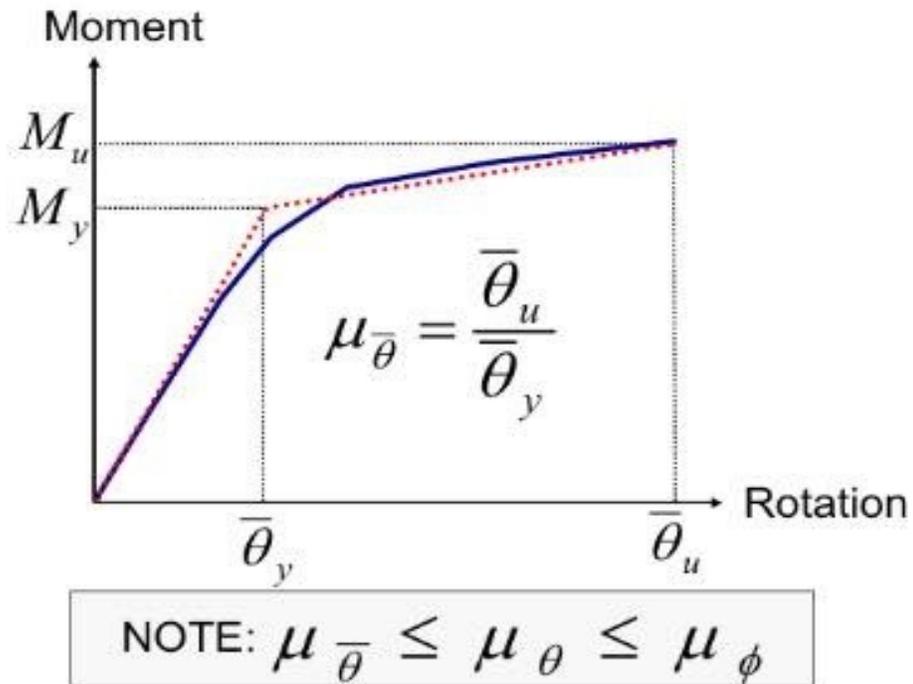


Elastic and Inelastic Behavior to Critical Region and Member

“critical region.” This region is that a part of the component over that vital inelastic behavior is predicted to occur. The important region coincides with the flexural plastic hinging of a beam. Once the applied member finish rotations square measure specified

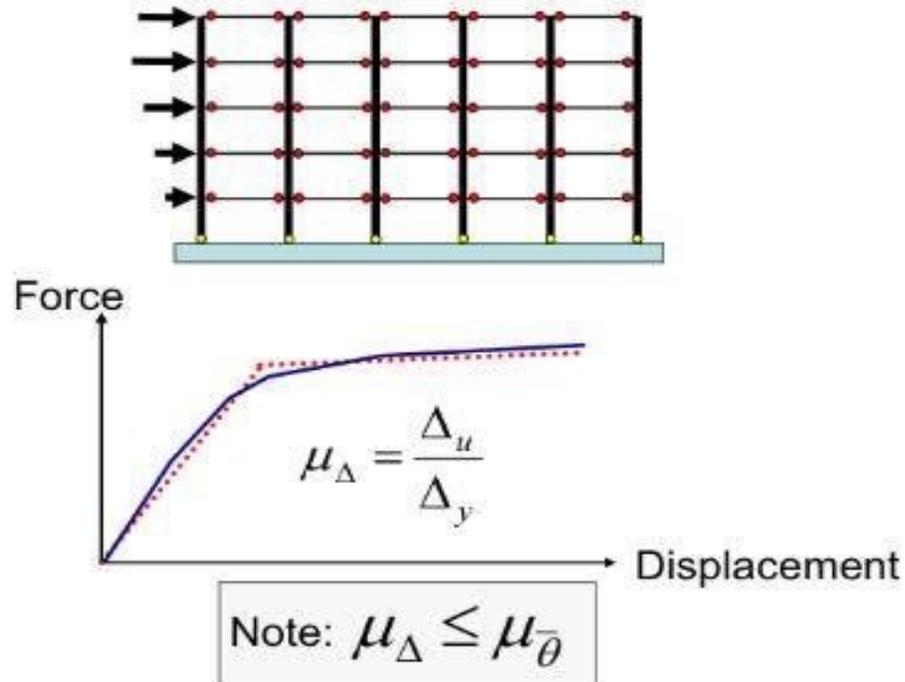
the yield moment is simply developed at the ends, the yield rotation within the hinging region may be shown. it's necessary, of course, to assume the length of this hinging region, that is around adequate the depth of the section.

When extra finish rotations square measure applied and also the final moments square measure developed at the member ends, inelastic curvature happens within the hinging region, and also the integration of those curvatures over the hinge length provides the inelastic rotation within the hinge [1].



Inelastic Behavior to Critical Region and Member

The rotational ductility SUPPLY is determined from the curve. Development of such curves is difficult, and requires static nonlinear analysis. the moment rotation relationship for a steel member is determined experimentally. The important thing to note is that inelastic buckling of the flanges has resulted (after a number of cycles) in a loss of moment capacity. However, this member is maintaining more that 10 percent of its capacity at rotations of 0.38 radians, which is approximately twice the limit allowed by the code. If the loss of strength was excessive, it would lead to a reduction in the available rotational ductility supply [1].



Inelastic Behavior to Structure

The overall response is given in terms of force and displacement. This curve is sometimes called a capacity curve or a pushover curve. The displacement ductility SUPPLY is as indicated [16].

3.1 Non-Adaptive Displacement-Based Pushover:

the modeling of earthquake moves as lateral displacements instead than forces constitutes a extra herbal and rational approach. Hence, there seems to exist a solid rationale for preferring the software of displacement alternatively than force patterns in pushover analysis. However, although conceptually sounder, serious sensible problems arise with traditional deformation-based pushover of buildings, in most cases due to the reality that the relative displacement between consecutive ground stages is fixed, for that reason concealing enormous structural characteristics and main to deceptive effects [17].

3.2 The Displacement-Based Adaptive Pushover Algorithm (DAP)

The displacement-based adaptive pushover algorithm adopted and developed within the modern-day work has been implemented in SeismoStruct two [14], a fiber-modeling Finite Element application for seismic evaluation of framed structures, which can be freely downloaded from the Internet. Full details on this laptop bundle can be located in its accompanying manual [15].

The implementation of the proposed algorithm can be structured in 4 major stages;

- (i) definition of nominal load vector and inertia mass,
- (ii) computation of load factor,
- (iii) calculation of normalized scaling vector and
- (iv) update of loading displacement vector.

Whilst the first step is carried out solely once, at the start of the analysis, its three final counterparts are repeated at every equilibrium stage of the nonlinear static evaluation procedure.

3.3 Capacity curves:

A series of top displacement versus base shear plots, comparatively illustrating static and dynamic results obtained for models with different structural characteristics subjected to equally diverse earthquake records, is given. It is also noted that, for the reasons provided in the companion paper, the dynamic analysis envelopes consist of the locus of maximum total drift versus corresponding base shear (i.e. peak base shear within a time-window ± 0.5 seconds of the instant of maximum drift occurrence) [15].

3.4 CREEP FAILURE

Failure of material can take place even under steady loads within the strength of the material. This happens if the subjected components remain under steady loads for a very longtime especially when they are subjected to high temperature conditions. Some common examples are stays in boilers, steam turbine blades, furnace parts etc. Such failures are termed creep-failures due to the fact the material continues to deform plastically under such conditions although at a very slow rate. But over long periods of time, the effect of creep can become appreciable resulting in ultimate failure of the component.

The purpose of this section is to show, somewhat informally, that the axiomatic structure set up in previous sections provides a rational basis for what is called "the internal variable approach" to plasticity [1, 2]. This approach may be briefly phrased as follows: In the internal variable theory of plasticity each state of a material is determined by the corresponding configuration G , plastic distortion D (which is an invertible linear transformation from Y onto σ) and by a vector α , the so called structural-parameter vector (α is an element of some finite-dimensional real vector space). The corresponding intrinsic stress is then given by

4. Conclusions:

The purpose of this study is to show and explain, somewhat informally, the inelastic behavior area in the stress-strain curve for different materials such as steel and concrete and effect this behavior on the structure of the construction.

An innovative displacement-based adaptive pushover procedure (DAP), whereby a set of laterally applied displacements, rather than forces, is monotonically applied to the structure, has been proposed. The novel algorithm, being fully displacement based, fits well within the current drive for the development and implementation of conceptually sounder nonlinear analysis tools for use within a performance and displacement-based design/assessment framework.

As far as the inner workings of the numerical algorithm is concerned, the main advantage of DAP resides on the fact that lateral deformations are directly determined through modal analysis that takes into consideration the stiffness state of the structure at each step, whilst storey shear force distributions result from the imposition of structural equilibrium at each analysis step. In this manner, response prediction limitations observed with force-based pushover methods are overcome.

◦. References:

1. Hawken, P., Lovins, A. B., & Lovins, L. H. (2013). *Natural capitalism: The next industrial revolution*. Routledge.
2. Williams, M. S., & Sexsmith, R. G. (1990). Seismic damage indices for concrete structures: a state-of-the-art review. *Earthquake spectra*, 11(2), 319-349.
3. Bammann, D. J., Chiesa, M. L., Horstemeyer, M. F., & Weingarten, L. I. (2010). Failure in ductile materials using finite element methods. *Structural crashworthiness and failure*, 1-04.
4. Kappos, A., & Penelis, G. G. (2010). *Earthquake resistant concrete structures*. CRC Press.
5. Moustafa, M. A. A. R. (2014). *Structural Behavior of Bent Cap Beams in As-built and Retrofitted Reinforced Concrete Box-Girder Bridges*. University of California, Berkeley.
6. Talukdar, S., Banthia, N., & Grace, J. R. (2012, September). The Effects of Structural Cracking on Carbonation Progress in Reinforced Concrete: Is Climate Change a Concern? In *Proceedings: 7rd International Conference on the Durability of Concrete Structures. Queens University Belfast, Sept* (pp. 17-19).
7. DeGarmo, E. P., Black, J. T., Kohser, R. A., & Klamecki, B. E. (1997). *Materials and process in manufacturing*. Prentice Hall.
8. Hufnagel, T. C., Schuh, C. A., & Falk, M. L. (2016). Deformation of metallic glasses: Recent developments in theory, simulations, and experiments. *Acta Materialia*, 109, 370-393.
9. Ashby, M. F., Evans, T., Fleck, N. A., Hutchinson, J. W., Wadley, H. N. G., & Gibson, L. J. (2000). *Metal foams: a design guide*. Elsevier.
10. Bazant, Z. P., & Planas, J. (1997). *Fracture and size effect in concrete and other quasibrittle materials* (Vol. 16). CRC press.
11. Chen, W. F. (2007). *Plasticity in reinforced concrete*. J. Ross Publishing.
12. Cairns, S. W. (2001). Circular concrete columns externally reinforced with pre-fabricated carbon polymer shells.
13. Sheikh, S. A., & Yeh, C. C. (1992). Analytical moment-curvature relations for tied concrete columns. *Journal of structural engineering*, 118(2), 029-044.
14. Priestley, M. N., Seible, F., & Calvi, G. M. (1996). *Seismic design and retrofit of bridges*. John Wiley & Sons.
15. Fiore, A., Spagnoletti, G., & Greco, R. (2016). On the prediction of shear brittle collapse mechanisms due to the infill-frame interaction in RC buildings under pushover analysis. *Engineering Structures*, 121, 147-109.

16 Crowley, H., Pinho, R., & Bommer, J. J. (2004). A probabilistic displacement-based vulnerability assessment procedure for earthquake loss estimation. *Bulletin of Earthquake Engineering*, 2(2), 173-219.

17. Antoniou, S., & Pinho, R. (2004). Development and verification of a displacement-based adaptive pushover procedure. *Journal of Earthquake Engineering*, 8(10), 643-661.